

**Listing of the Claims:**

Below is a listing of all claims using a strikethrough and underlining to show changes.

- 1.(original) A quasi-resonant buck converter comprising:
  - 5 a) a connection point;
  - b) a top switch connected to a power source and to the connection point;
  - c) a auxiliary switch connected to the connection point and to a return potential;
  - d) a resonant inductor connected to the connection point and to an output inductor;
  - e) a resonant capacitor connected to the return potential and to the resonant inductor,
  - 10 whereby the resonant inductor and resonant capacitor are connected in series across the auxiliary switch;
  - f) a synchronous switch connected in parallel with the resonant capacitor.
- 2.(original) The buck converter of claim 1, wherein the resonant inductor has an
 - 15 inductance value in the range of 1-10000 nH.
- 3.(original) The buck converter of claim 1, wherein the resonant capacitor has a
 - capacitance value in the range of 0.01-100  $\mu$ F.
- 20 4.(original) The buck converter of claim 1, wherein the quantity  $\frac{3}{2}\pi\sqrt{LC}$  is in the range of 0.05 to 5 microseconds, where L is the inductance of the resonant inductor, and C is the capacitance of the resonant capacitor.
- 5.(original) The buck converter of claim 1, further comprising a switch controller for
 - 25 controlling the synchronous switch, wherein the switch controller can phase shift the operation of the synchronous switch to control output power.
- 6.(currently amended) The buck converter of claim 1, further comprising a switch controller for controlling the ~~gate~~ synchronous switch, and wherein the switch

controller operates the synchronous switch so that an ON time of the synchronous switch is equal to an OFF time of the synchronous switch.

- 5 7.(original) The buck converter of claim 1, further comprising a switch controller, and wherein the switch controller operates the synchronous switch so that an OFF time of the synchronous switch is approximately equal to  $\frac{3}{2}\pi\sqrt{LC}$ , where L is the inductance of the resonant inductor, and C is the capacitance of the resonant capacitor.
- 10 8.(original) A quasi-resonant tap-buck converter comprising:
- a) a connection point;
  - b) a top switch connected to a power source and to the connection point;
  - c) a auxiliary switch connected to a return potential;
  - d) a clamping capacitor connected to the auxiliary switch and to the connection point;
  - 15 e) a resonant inductor connected to the connection point;
  - f) primary and secondary coupled inductors connected in series with a parallel polarity, with the primary inductor connected to the resonant inductor;
  - g) a resonant capacitor connected between the return potential and a midpoint of the coupled inductors ;
  - 20 h) a synchronous switch connected in parallel with the resonant capacitor.
9. (original) The buck converter of claim 8, wherein the primary coupled inductor has an inductance value in the range of 1-10000 nH.
- 25 10.(original) The buck converter of claim 8, wherein the resonant capacitor has a capacitance value in the range of 0.01-100  $\mu$ F.
11. (original) The buck converter of claim 8, wherein the quantity  $\frac{3}{2}\pi\sqrt{(L+Lk)C}$  is in the range of 0.05 to 5 microseconds, where L is the inductance of the resonant

inductor,  $L_k$  is the leakage inductance of the primary coupled inductor, and  $C$  is the capacitance of the resonant capacitor.

12. (original) The buck converter of claim 8, further comprising a switch controller that  
5 can vary the duration of a time period  $A$  and thereby control an output power.

13. (original) The buck converter of claim 8, further comprising a switch controller that  
can vary the combined duration of a time periods  $A$  and  $B$  and thereby control an  
output voltage.

14. (original) The buck converter of claim 8, further comprising a switch controller that  
controls the circuit such that an OFF time for the synchronous switch is  
approximately equal to  $\frac{3}{2}\pi\sqrt{(L + L_k)C}$ , where  $L$  is the inductance of the resonant  
inductor,  $L_k$  is the leakage inductance of the primary coupled inductor, and  $C$  is  
15 the capacitance of the resonant capacitor.

15.(original) A quasi-resonant isolated converter comprising:

- a) a connection point;
- b) a top switch connected to a power source and to the connection point;
- 20 c) a auxiliary switch connected to a return potential;
- d) a clamping capacitor connected to the auxiliary switch and to the connection point;
- e) a resonant inductor connected to the connection point;
- f) a transformer with a primary winding connected between the resonant inductor and the  
return potential, and with a secondary winding;
- 25 g) a synchronous switch connected in series with the secondary winding;
- h) a resonant capacitor connected in parallel with the synchronous switch.

16. (original) The buck converter of claim 15, wherein the resonant inductor has an  
inductance value in the range of 1-10000 nH.

17. (original) The buck converter of claim 15, wherein the resonant capacitor has a capacitance value in the range of 0.01-100  $\mu\text{F}$ .

18. (original) The buck converter of claim 15, wherein the quantity  $\frac{3}{2}\pi\frac{N_s}{N_p}\sqrt{(L+L_k)C}$  is

5 in the range of 0.05 to 5 microseconds, where L is the inductance of the resonant inductor,  $L_k$  is the leakage inductance of the transformer, C is the capacitance of the resonant capacitor,  $N_s$  is the number of turns in the secondary winding, and  $N_p$  is the number of turns in the primary winding.

10 19. (original) The buck converter of claim 15, further comprising a switch controller that can vary the duration of a time period A and thereby control the output power.

15 20. (original) The buck converter of claim 15, further comprising a switch controller that can vary the combined duration of a time periods A and B and thereby control the output voltage.

21. (original) The buck converter of claim 15, further comprising a switch controller that controls the circuit such that an OFF time for the synchronous switch is approximately equal to  $\frac{3}{2}\pi\frac{N_s}{N_p}\sqrt{(L+L_k)C}$ , where L is the inductance of the  
20 resonant inductor,  $L_k$  is the leakage inductance of the transformer, C is the capacitance of the resonant capacitor,  $N_s$  is the number of turns in the secondary winding, and  $N_p$  is the number of turns in the primary winding.

25 22. (original) The buck converter of claim 15 wherein the transformer has a  $N_p/N_s$  turns ratio of at least 4:1.

23. (new) The buck converter of claim 1 wherein there is not a diode in series with the resonant inductor.

24. (new) The buck converter of claim 8 wherein there is not a diode in series with the resonant inductor.

5 25. (new) The buck converter of claim 15 wherein there is not a diode in series with the resonant inductor.